

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate only, other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (07804-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (LEAVE BLANK)		2. REPORT DATE  1998		3. REPORT TYPE AND DATES COVERED  Professional Paper
4. TITLE AND SUBTITLE Scattering By Electrically Large Objects With Cavity-Like Features		5. FUNDING NUMBERS		
6. AUTHOR(S) Stuart W. Altizer, John S. Asvestas and James M. Stamm				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)  Naval Air Warfare Center Aircraft Division 22347 Cedar Point Road, Unit #6 Patuxent River, Maryland 20670-1161		8. PERFORMING ORGANIZATION REPORT NUMBER		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSORING/MONITORING AGENCY REPORT NUMBER		
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION/AVAILABILITY STATEMENT  Approved for public release; distribution is unlimited.		12b. DISTRIBUTION CODE		
13. ABSTRACT (Maximum 200 words)				
14. SUBJECT TERMS			15. NUMBER OF PAGES	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT  Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE  Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT  Unclassified	20. LIMITATION OF ABSTRACT  SAR	

# SCATTERING BY ELECTRICALLY LARGE OBJECTS WITH CAVITY-LIKE FEATURES.

A HYBRID APPROACH.

CLEARED FOR  
OPEN PUBLICATION

JUN 3 1998

PUBLIC AFFAIRS OFFICE  
NAVAL AIR SYSTEMS COMMAND

by.

*A. Hovuz*

Stuart W. Altizer, John S. Asvestas and James M. Stamm.  
RF Sensors Branch.

Naval Air Warfare Center – Aircraft Division.

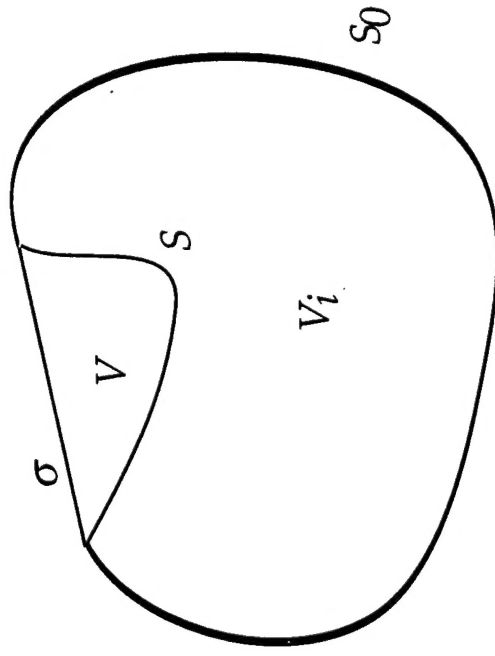
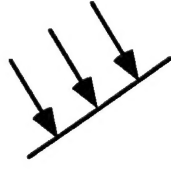
19980810 077

DTIC QUALITY INSPECTED 1

Page: 1

# THE PROBLEM: LARGE SCATTERER WITH A CAVITY

Incident  
plane wave propagating  
in free space.  
Harmonic ( $\exp[-i\omega t]$ )  
time dependence.  
Incident fields:  $E^i, H^i$



Scattered fields:  $E^s, H^s$

Total fields in exterior:

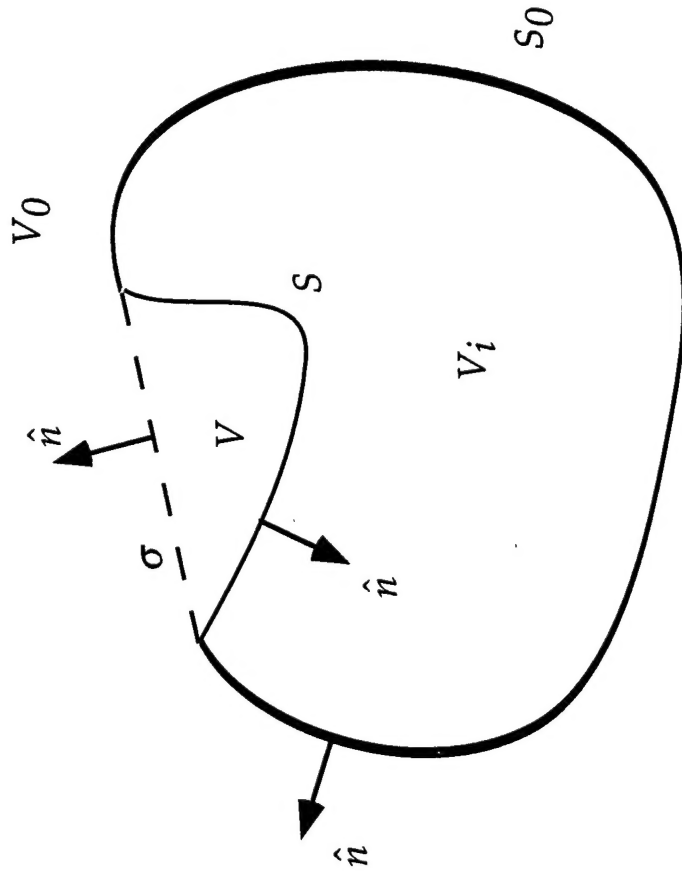
$$E^t = E^i + E^s$$

$$H^t = H^i + H^s$$

Total fields in  $V$  :  $E, H$

The closed surface  $S \cup S_0$   
is perfectly conducting.  
Constitutive parameters in  $V$   
are arbitrary.

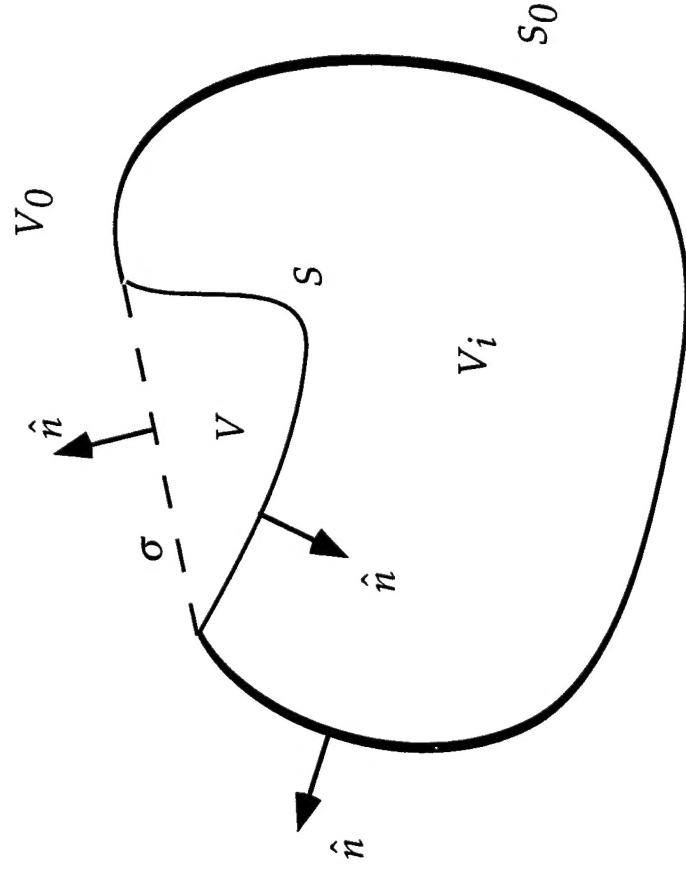
## ANOTHER LOOK AT THE GEOMETRY



- CAVITY SIZE EXAGGERATED
  - SURFACE  $S \cup S_0$  IS VERY MANY SQUARE WAVELENGTHS IN AREA
- $\Rightarrow$  A HYBRID METHOD IS CALLED FOR.

## SPECIFICALLY

- USE A HIGH-FREQUENCY METHOD FOR THE LARGE PART OF THE STRUCTURE ( $S_0$ )
- USE THE METHOD OF MOMENTS IN THE CAVITY ( $V$ )
- COUPLE THE TWO AT THE ENTRANCE,  $\sigma$ , TO THE CAVITY



## MOST RECENT HYBRID APPROACH TO THIS PROBLEM

Jin, J.-M., Ni, S.S. and Lee, S.W., "Hybridization of SBR and FEM for scattering by large bodies with cracks and cavities", *IEEE Trans. Antennas Propagat.*, Vol. 43 (10), pp. 1130-1139, Oct. 1995

SBR: Shooting and bouncing rays; FEM: Finite element method

PRINCIPAL DIFFERENCE BETWEEN THIS METHOD AND THE ONE WE WILL DESCRIBE IS IN THE KIND OF GREEN'S FUNCTION (GF) THEY USE:

- THE SBR/FEM USES A SPECIALIZED GF
- OUR METHOD USES THE FREE SPACE GF

## FREE SPACE DYADIC GREEN'S FUNCTION

$$\underline{\Gamma}(k; \mathbf{r}, \mathbf{r}') = ik\nabla \times [G(k; \mathbf{r}, \mathbf{r}')\underline{\mathbf{I}}] \quad , \quad G(k; \mathbf{r}, \mathbf{r}') = -e^{ikR} / 4\pi R \quad , \quad R = |\mathbf{r} - \mathbf{r}'|$$

•IT SATISFIES

$$\nabla \times \nabla \times \underline{\Gamma}(k; \mathbf{r}, \mathbf{r}') - k^2 \underline{\Gamma}(k; \mathbf{r}, \mathbf{r}') = -ik\nabla \times [\delta(\mathbf{r}, \mathbf{r}')\underline{\mathbf{I}}]$$

•AND CAN BE INTERPRETED AS

•THE MAGNETIC FIELD OF THREE ORTHOGONALLY CROSSED ELECTRIC  
DIPOLES

OR

•AS THE ELECTRIC FIELD OF THREE ORTHOGONALLY CROSSED  
MAGNETIC DIPOLES

•AND IT IS VERY EASY TO COMPUTE

## DYADICS OF THE FIRST AND SECOND KIND

•USING  $\underline{\Gamma}$  WE CAN CONSTRUCT DYADICS  $\underline{\Gamma}_1$  AND  $\underline{\Gamma}_2$  THAT SATISFY

$$\hat{n} \times \underline{\Gamma}_1(k; \mathbf{r}, \mathbf{r}') = 0 \quad , \quad \hat{n} \times \nabla \times \underline{\Gamma}_2(k; \mathbf{r}, \mathbf{r}') = 0$$

ON SOME SURFACE S.

•IF S IS PERFECTLY CONDUCTING, THEN  $\underline{\Gamma}_1$  IS AN ELECTRIC FIELD WHILE  $\underline{\Gamma}_2$  IS A MAGNETIC FIELD.

•WE CAN WRITE FOR THESE DYADICS

$$\underline{\Gamma}_1 = \underline{\Gamma} + \underline{\Gamma}_1^S \quad \text{AND} \quad \underline{\Gamma}_2 = \underline{\Gamma} + \underline{\Gamma}_2^S$$

- THUS TO DETERMINE THESE DYADICS WE MUST FIND THE FIELDS OF INFINITESIMAL DIPOLES IN THE PRESENCE OF A PERFECT CONDUCTOR.
- THIS IS A MORE DIFFICULT UNDERTAKING THAN THE ORIGINAL PROBLEM IF THE SCATTERER IS GEOMETRICALLY COMPLEX.
- FOR THIS REASON WE PREFER AN APPROACH THAT USES THE *FREE-SPACE* GREEN'S FUNCTION.



## PROPOSED METHOD

• THE MAGNETIC FIELD IN  $V_0$

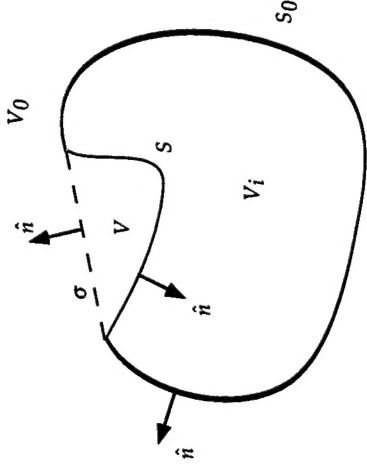
$$\mathbf{H}^s(\mathbf{r}') = \frac{\gamma_0}{k_0^2} \int_{\sigma} \left\{ \left[ \hat{\mathbf{n}} \times \mathbf{E}^t(\mathbf{r}) \right] \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Z_0 \left[ \hat{\mathbf{n}} \times \mathbf{H}^t(\mathbf{r}) \right] \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS \\ + \frac{i}{k_0} \int_{S_0} \left[ \hat{\mathbf{n}} \times \mathbf{H}^t(\mathbf{r}) \right] \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in V_0$$

• LET

$$\mathbf{J}_{S_0}^t(\mathbf{r}) = \hat{\mathbf{n}} \times \mathbf{H}^t(\mathbf{r}), \quad \mathbf{r} \in S_0; \quad \mathbf{M}_{\sigma}^t(\mathbf{r}) = -\hat{\mathbf{n}} \times \mathbf{E}^t(\mathbf{r}), \quad \mathbf{J}_{\sigma}^t(\mathbf{r}) = \hat{\mathbf{n}} \times \mathbf{H}^t(\mathbf{r}), \quad \mathbf{r} \in \sigma$$

• THEN

$$\mathbf{H}^t(\mathbf{r}') = \mathbf{H}^{inc}(\mathbf{r}') + \frac{\gamma_0}{k_0^2} \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Z_0 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS \\ + \frac{i}{k_0} \int_{S_0} \mathbf{J}_{S_0}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in V_0$$



•MAKE A HIGH-FREQUENCY APPROXIMATION TO THE SURFACE CURRENT ON  $S_0$

$$\mathbf{H}_0^t(\mathbf{r}') = \frac{i}{k_0} \int_{S_0^*} \mathbf{J}_{S_0}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in V_0$$

$$\mathbf{H}^{kn}(\mathbf{r}') = \mathbf{H}^{inc}(\mathbf{r}') + \mathbf{H}_0^t(\mathbf{r}'), \quad \mathbf{r}' \in V_0$$

•THEN

$$\mathbf{H}^t(\mathbf{r}') = \mathbf{H}^{kn}(\mathbf{r}')$$

$$+ \frac{\gamma_0}{k_0^2} \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Z_0 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS, \quad \mathbf{r}' \in V_0$$

•SIMILARLY

$$\mathbf{E}^t(\mathbf{r}') = \mathbf{E}^{kn}(\mathbf{r}')$$

$$- \frac{Z_0}{k_0^2} \int_{\sigma} \left\{ \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Y_0 \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS, \quad \mathbf{r}' \in V_0$$

•WITH

$$\mathbf{E}^{kn}(\mathbf{r}') = \mathbf{E}^{inc}(\mathbf{r}') + \mathbf{E}_0^t(\mathbf{r}'), \quad \mathbf{E}_0^t(\mathbf{r}') = -\frac{Z_0}{k_0^2} \int_{S_0^*} \mathbf{J}_{S_0}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in V_0$$

# INTEGRAL REPRESENTATIONS IN V

•WITH  $\mathbf{J}_S(\mathbf{r}) = -\hat{n} \times \mathbf{H}(\mathbf{r})$  ,  $\mathbf{r} \in S$

•AND THE TRANSMISSION AND BOUNDARY CONDITIONS

$\mathbf{M}_\sigma^t(\mathbf{r}) = -\hat{n} \times \mathbf{E}(\mathbf{r})$ ,  $\mathbf{J}_\sigma^t(\mathbf{r}) = \hat{n} \times \mathbf{H}(\mathbf{r})$ ,  $\mathbf{r} \in \sigma$ ;  $\hat{n} \times \mathbf{E}(\mathbf{r}) = 0$ ,  $\mathbf{r} \in S$

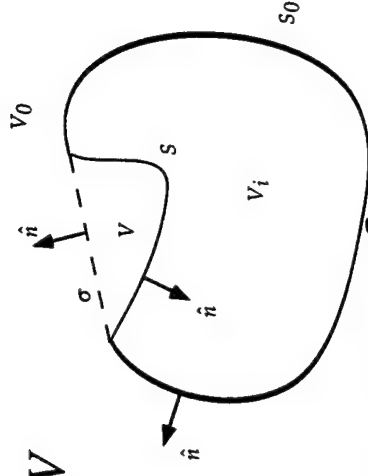
•WE GET

$$\mathbf{H}(\mathbf{r}') = -\frac{\gamma_1}{k_1} \frac{1}{2} \int_\sigma \left\{ -\mathbf{M}_\sigma^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 Z_1 \mathbf{J}_\sigma^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS$$

$$+ \frac{i}{k_1} \int_S \mathbf{J}_S(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS \quad , \quad \mathbf{r}' \in V$$

$$\mathbf{E}(\mathbf{r}') = \frac{Z_1}{k_1} \frac{1}{2} \int_\sigma \left\{ \mathbf{J}_\sigma^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 \gamma_1 \mathbf{M}_\sigma^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS$$

$$- \frac{Z_1}{k_1} \frac{1}{2} \int_S \mathbf{J}_S(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS \quad , \quad \mathbf{r}' \in V$$



# FROM INTEGRAL REPRESENTATIONS TO INTEGRAL EQUATIONS

• LET  $\mathbf{r}'$  APPROACH A POINT ON  $\sigma$  FROM  $V_0$

$$\frac{1}{2} \mathbf{J}_{\sigma}^t(\mathbf{r}') = \mathbf{J}_{\sigma}^{kn}(\mathbf{r}')$$

$$+ \frac{\gamma_0}{k_0^2} \hat{n}' \times \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Z_0 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS, \mathbf{r}' \in \sigma$$

$$\frac{1}{2} \mathbf{M}_{\sigma}^t(\mathbf{r}') = \mathbf{M}_{\sigma}^{kn}(\mathbf{r}')$$

$$+ \frac{Z_0}{k_0^2} \hat{n}' \times \int_{\sigma} \left\{ \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') + ik_0 Y_0 \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') \right\} dS, \mathbf{r}' \in \sigma$$

• WHERE

$$\mathbf{M}_{\sigma}^{kn}(\mathbf{r}) = -\hat{n} \times \mathbf{E}^{kn}(\mathbf{r}), \quad \mathbf{J}_{\sigma}^{kn}(\mathbf{r}) = \hat{n} \times \mathbf{H}^{kn}(\mathbf{r}), \quad \mathbf{r} \in \sigma$$

•LET  $\mathbf{r}'$  APPROACH A POINT ON  $\sigma$  FROM  $V_i$

$$\begin{aligned} \frac{1}{2} \mathbf{J}_{\sigma}^t(\mathbf{r}') = & -\frac{\gamma_1}{k_1^2} \hat{n}' \times \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 Z_1 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS \\ & + \frac{i}{k_1} \hat{n}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in \sigma \end{aligned}$$

$$\begin{aligned} -\frac{1}{2} \mathbf{M}_{\sigma}^t(\mathbf{r}') = & \frac{Z_1}{k_1^2} \hat{n}' \times \int_{\sigma} \left\{ \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 \gamma_1 \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS \\ & - \frac{Z_1}{k_1^2} \hat{n}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in \sigma \end{aligned}$$

•LET  $\mathbf{r}'$  APPROACH A POINT ON  $S$  FROM  $V_i$

$$-\frac{1}{2}\mathbf{J}_S(\mathbf{r}') = -\frac{\gamma_1}{k_1^2}\hat{\mathbf{n}}' \times \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 Z_1 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS \\ + \frac{i}{k_1} \hat{\mathbf{n}}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS \quad , \quad \mathbf{r}' \in S$$

$$0 = \hat{\mathbf{n}}' \times \int_{\sigma} \left\{ \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 \gamma_1 \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS \\ - \hat{\mathbf{n}}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS \quad , \quad \mathbf{r}' \in S$$

## A SYSTEM OF EQUATIONS

•FOR OBSERVATION POINTS ON  $S$

$$\begin{aligned}
 -\frac{1}{2}\mathbf{J}_S(\mathbf{r}') = & -\frac{\gamma_1}{k_1}\frac{1}{2}\hat{n}' \times \int_{\sigma} \left\{ -\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') + ik_1 Z_1 \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') \right\} dS \\
 & + \frac{i}{k_1} \hat{n}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in S
 \end{aligned}$$

•FOR OBSERVATION POINTS ON  $\sigma$

$$\begin{aligned}
 \frac{i}{2}(k_0 Z_0 + k_1 Z_1) \mathbf{J}_{\sigma}^t(\mathbf{r}') &= ik_0 Z_0 \mathbf{J}_{\sigma}^{kn}(\mathbf{r}') \\
 &+ \hat{n}' \times \int_{\sigma} \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \left[ \frac{\nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}')}{ik_0} - \frac{\nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}')}{ik_1} \right] dS \\
 &- \hat{n}' \times \int_{\sigma} \mathbf{J}_{\sigma}^t(\mathbf{r}) \cdot [Z_0 \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') - Z_1 \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}')] dS \\
 &- Z_1 \hat{n}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in \sigma
 \end{aligned}$$

•FOR OBSERVATION POINTS ON  $\sigma$

$$\begin{aligned}
 \frac{i}{2}(k_0\gamma_0 + k_1\gamma_1)\mathbf{M}_\sigma^t(\mathbf{r}') &= ik_0\gamma_0\mathbf{M}_\sigma^{kn}(\mathbf{r}') \\
 -\hat{n}' \times \int_\sigma \mathbf{J}_\sigma^t(\mathbf{r}) \cdot &\left[ \frac{\nabla \times \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}')}{ik_0} - \frac{\nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}')}{ik_1} \right] dS \\
 -\hat{n}' \times \int_\sigma \mathbf{M}_\sigma^t(\mathbf{r}) \cdot &[\gamma_0 \underline{\Gamma}(k_0; \mathbf{r}, \mathbf{r}') - \gamma_1 \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}')] dS \\
 + \frac{i}{k_1} \hat{n}' \times \int_S \mathbf{J}_S(\mathbf{r}) \cdot &\nabla \times \underline{\Gamma}(k_1; \mathbf{r}, \mathbf{r}') dS \quad , \quad \mathbf{r}' \in \sigma
 \end{aligned}$$



# IN NON-DYADIC FORM

$$-\frac{1}{2}\mathbf{J}_S(\mathbf{r}') = \frac{i\chi_1}{k_1}\hat{\mathbf{n}}' \times \int_{\sigma} [\mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot \nabla \nabla G(k_1; \mathbf{r}, \mathbf{r}') + k_1^2 G(k_1; \mathbf{r}, \mathbf{r}') \mathbf{M}_{\sigma}^t(\mathbf{r})] dS \\ + \hat{\mathbf{n}}' \times \int_{\sigma} [\mathbf{J}_{\sigma}^t(\mathbf{r}) \times \nabla G(k_1; \mathbf{r}, \mathbf{r}')] dS - \hat{\mathbf{n}}' \times \int_S \mathbf{J}_S(\mathbf{r}) \times \nabla G(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in S$$

$$\frac{i}{2}(k_0 Z_0 + k_1 Z_1) \mathbf{J}_{\sigma}^t(\mathbf{r}') = ik_0 Z_0 \mathbf{J}_{\sigma}^{kn}(\mathbf{r}') \\ + \hat{\mathbf{n}}' \times \int_{\sigma} \mathbf{M}_{\sigma}^t(\mathbf{r}) \cdot [\nabla \nabla G(k_0; \mathbf{r}, \mathbf{r}') - \nabla \nabla G(k_1; \mathbf{r}, \mathbf{r}')] dS \\ + \hat{\mathbf{n}}' \times \int_{\sigma} \mathbf{M}_{\sigma}^t(\mathbf{r}) [k_0^2 G(k_0; \mathbf{r}, \mathbf{r}') - k_1^2 G(k_1; \mathbf{r}, \mathbf{r}')] dS \\ + \hat{\mathbf{n}}' \times \int_{\sigma} \mathbf{J}_{\sigma}^t(\mathbf{r}) \times \nabla [k_0 Z_0 G(k_0; \mathbf{r}, \mathbf{r}') - k_1 Z_1 G(k_1; \mathbf{r}, \mathbf{r}')] dS \\ - ik_1 Z_1 \hat{\mathbf{n}}' \times \int_S \mathbf{J}_S(\mathbf{r}) \times \nabla G(k_1; \mathbf{r}, \mathbf{r}') dS, \quad \mathbf{r}' \in \sigma$$

$$\begin{aligned}
& \frac{i}{2}(k_0\gamma_0 + k_1\gamma_1)\mathbf{M}_\sigma^t(\mathbf{r}') = ik_0\gamma_0\mathbf{M}_\sigma^{kn}(\mathbf{r}') \\
& -\hat{n}' \times \int_{\sigma} \mathbf{J}_\sigma^t(\mathbf{r}) \cdot [\nabla\nabla G(k_0;\mathbf{r},\mathbf{r}') - \nabla\nabla G(k_1;\mathbf{r},\mathbf{r}')] dS \\
& -\hat{n}' \times \int_{\sigma} \mathbf{J}_\sigma^t(\mathbf{r}) [k_0^2 G(k_0;\mathbf{r},\mathbf{r}') - k_1^2 G(k_1;\mathbf{r},\mathbf{r}')] dS \\
& -i\hat{n}' \times \int_{\sigma} \mathbf{M}_\sigma^t(\mathbf{r}) \times \nabla [k_0\gamma_0 G(k_0;\mathbf{r},\mathbf{r}') - k_1\gamma_1 G(k_1;\mathbf{r},\mathbf{r}')] dS \\
& -\hat{n}' \times \int_S \{ \mathbf{J}_S(\mathbf{r}) \cdot \nabla\nabla G(k_1;\mathbf{r},\mathbf{r}') + k_1^2 G(k_1;\mathbf{r},\mathbf{r}') \mathbf{J}_S(\mathbf{r}) \} dS, \quad \mathbf{r}' \in \sigma
\end{aligned}$$

## SOME OBSERVATIONS ON THE NUMERICAL IMPLEMENTATION

•NOTE THAT

$$\begin{aligned} \nabla \nabla [G(k_0; \mathbf{r}, \mathbf{r}') - G(k_1; \mathbf{r}, \mathbf{r}')] &= \frac{1}{4\pi} \nabla \nabla \left[ \frac{e^{ik_1 R}}{R} - \frac{e^{ik_0 R}}{R} \right] \\ &= \frac{1}{4\pi} \left[ \frac{k_0^2 - k_1^2}{2R} (\mathbf{I} - \hat{R}\hat{R}) + O(R^0) \right], \quad R = |\mathbf{r} - \mathbf{r}'| \rightarrow 0 \end{aligned}$$

- THUS, THE ENTIRE TERM ABOVE BEHAVES AS A SIMPLE LAYER POTENTIAL.
- THIS ALLOWS US TO USE A COLLOCATION METHOD (PULSE BASIS AND DELTA TESTING FUNCTIONS).
- ALTERNATIVELY, GLISSON'S BASIS AND TESTING FUNCTIONS MAY BE USED.

## CLOSING REMARKS

- ANY OTHER COMBINATION OF THE INTEGRAL EQUATIONS ON  $\sigma$  IS NOT RECOMMENDED
  - SPECIFICALLY, EFIE-TYPE EQUATIONS REQUIRE A HIGH-FREQUENCY APPROXIMATION OF THE CHARGE DENSITY ALSO.
  - THE PERFECTLY CONDUCTING (LARGE) PART OF THE SCATTERER CAN BE REPLACED BY ONE SATISFYING AN IBC.
-